

[4] involute ASM (high-intensity gear design system)

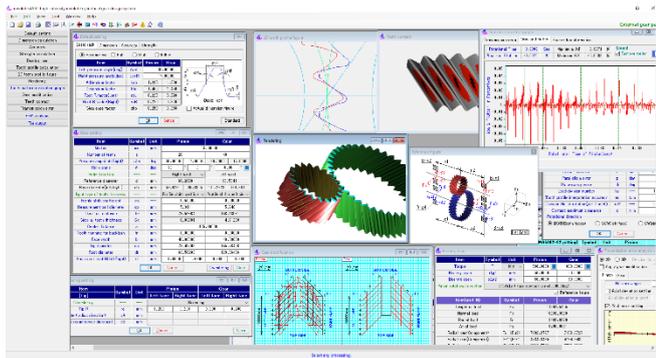


Fig. 4.1 involute ASM (high-intensity gear/asymmetry gear)

4.1 Abstract

This software is design support software for asymmetric pressure angle involute gear (hereinafter referred to as asymmetric gear). The whole screen is shown in Figure 4.1. Asymmetrical gears can increase tooth load capacity without changing gear size or material. Compared with standard pressure angle, high pressure square teeth have lower Hertz stress, smaller friction coefficient, smaller slip ratio, and lower flash temperature.

4.2 Software structure

The configuration of involute ASM is shown in Table 4.1. "○" in the table is included in the basic software, "◎" is optional.

Type of gear: involute gear, external and internal gear

Table 4.1 software structure

Item	Structure
<1> Basic rack	○
<2> Gear dimension	○
<3> Inference	○
<4> Tooth creation drawing	○
<5> Meshing drawing	○
<6> Meshing rotation function	○
<7> Tooth profile (DXF file)	○
<8> Tooth profile rendering	○
<9> Gear accuracy	○
<10> Design data management	○
<11> JGMA6101,6102, JGMA401,402	○
<12> Metal × plastic gear strength (JIS B 1759)	○
<13> Bearing load	○
<14> Tooth profile (3D-IGES file)	○
<15> Rotational transmission error (Fourier analysis, Wow · flutter, CSV output)	◎
<16> Tooth modification (involute, lead, bias)	◎
<17> Contact pattern	◎
<18> FEM Tooth Profile Analysis	◎

4.3 Property (Basic rack, accuracy, strength)

Setup screen is shown in Fig.4.2~4.5.

- gear combination : external × external, external × internal
- Basic rack : normal, low, special
- tooth tip circle decision : normal, equal clearance
- There are two types of strength calculation standards for steel gears as shown in Figure 4.5.

- JGMA 401-02:1974, 402-02:1975
- JGMA 6101-02:2007, 6102-02:2009

In addition, the strength calculation standard of plastic gears corresponds to JIS B 1759 (2013).

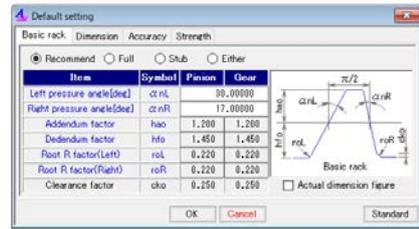


Fig. 4.2 Basic rack (asymmetry)

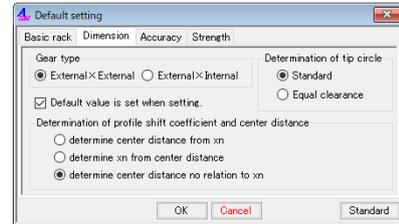


Fig. 4.3 Dimension

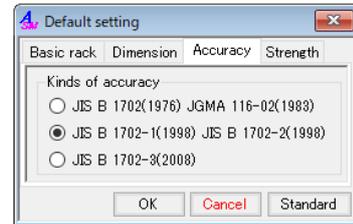


Fig. 4.4 Accuracy

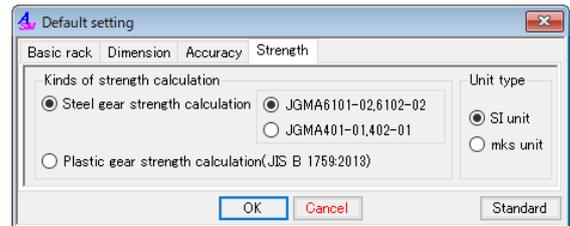


Fig. 4.5 Strength

4.4 Gear dimension

The gear dimensions calculate the dimensions, contact ratio, sliding ratio, tooth thickness, etc.. The contact ratio of the undercut-generated gear is calculated based on the True Involute form (TIF) diameter. Also, if the tip is rounded, the contact ratio is calculated taking into account the tip R.

- (1) The relationship between center distance and dislocation coefficient is the following three types.
 - (1.1) The profile shift factor is given to the pinion and gear to determine the center distance.
 - (1.2) A profile shift factor is given to each gear based on the center distance.
 - (1.3) The center distance is arbitrarily determined ignoring the profile shift factor.
- (2) There are 4 types of setting method of profile shift factor as follows.
 - (2.1) Input the profile shift factor directly to each gear.
 - (2.2) Input the over pin size and determine the profile shift factor.

However, in the case of asymmetric gear, it is not possible to the span measurement.

 - (2.3) The arc tooth thickness is input to determine the profile shift factor.

Fig. 4.6 shows the gear specification setting screen.

Fig. 4.8 shows the dimension result screen when the tooth tip R is set to 0.2 (C surface is also possible) with the chamfering setting shown in Fig. 4.7.

Item	Symbol	Unit	Pinion	Gear
Module	m	mm	3.00000	
Number of teeth	z	---	20	40
Pressure angle(left/right)	α_n	deg	30.0000	17.0000
Helix angle	β	deg	30	0
Helix direction	---	---	Right hand	Left hand
Reference diameter	d	mm	69.28203	138.56406
Base diameter(left/right)	db	mm	57.6461	65.3305
Input type of tooth thickness	---	---	Profile shift coefficient	Profile shift coefficient
Profile shift coefficient	xn	---	0.50000	Profile shift coefficient
Measurement ball diameter	dp	mm	5.311	Ball diameter
Over ball distance	dm	mm	79.52664	146.13031
Circular tooth thickness	Sn	mm	6.03701	4.71239
Center distance	a	mm	105.60000	
Tooth thinning for backlash	fn	mm	0.00000	0.00000
Face width	b	mm	40.00000	40.00000
Tip diameter	da	mm	79.48203	145.76406
Root diameter	df	mm	63.58203	129.86406
Basic rack root R(left/right)	rf	mm	0.6600	0.6600

Fig. 4.6 Gear dimensions

Item	Symbol	Unit	Pinion	Gear
Chamfering	---	---	Rounding	
Tip R	ra	mm	0.200	0.200
Chamfer(radius direction)	cA	mm		
Chamfer(circumference direction)	cB	mm		

Fig. 4.7 Chamfering setting

Item	Symbol	Unit	Pinion	Gear
Transverse module	mt	mm	3.46410	
Transverse pressure angle	α_{t1}	deg	33.6901	19.4444
Effective face width	bw	mm	40.0000	
Lead	pz	mm	378.9911	753.9822
Profile shift amount	Xm	mm	1.50000	0.00000
Addendum	ha	mm	5.1000	3.6000
Dedendum	hf	mm	2.8500	4.3500
Tooth depth	h	mm	7.9500	7.9500
Clearance	c	mm	0.9270	0.9270
Contact diameter(tip)	d _{sa}	mm	79.3564	79.3076
Contact diameter(root)	d _{sf}	mm	66.0763	66.3392
Base cylindrical helix angle	β_b	deg	25.6589	28.5648
Transverse contact pressure angle	α_{w1}	deg	35.0314	21.8763
Contact pitch diameter	d _w	mm	70.4000	140.8000
Transverse pitch	p _{bt}	mm	9.0550	10.2621
Normal pitch	p _{bn}	mm	8.1621	9.0130
Contact length	ea	mm	11.1190	15.1877
Transverse contact ratio	$\epsilon_{\alpha 1}$	---	1.2279	1.4800
Overlap contact ratio	ϵ_{β}	---	2.1221	
Total contact ratio	ϵ_{γ}	---	3.3500	3.6020
Lowest point contact ratio	$\epsilon_{\alpha L}$	---	0.7800	0.9126
Highest point contact ratio	$\epsilon_{\alpha H}$	---	0.4479	0.5674
Sliding ratio(tip)	σ_a	---	0.3871	0.6249
Sliding ratio(root)	σ_b	---	-0.3703	-1.1974
Over ball distance	d _m	mm	79.5266	146.1303
Normal circular tooth thickness	s _n	mm	6.0370	4.7124
Transverse circular tooth thickness	s _t	mm	6.9709	5.4414
Chordal height	h _j	mm	5.2123	3.6300
Chordal tooth thickness(Reference)	S _j	mm	6.0327	4.7119
Addendum factor of basic rack	ha ₀	---	1.2000	1.2000
Dedendum factor of basic rack	hf ₀	---	1.4500	1.4500
Backlash	jt	mm	0.2402	
Transverse backlash	j _{tn}	mm	0.1967	0.2229

Fig. 4.8 Gear dimension result

4.6 Tooth profile

Tooth profile calculation can give division numbers to each tooth profile as shown in Figure 4.9. Then calculate the left and right tooth profile with "Tooth profile calculation" and show the tooth profile as shown in Fig. 4.10. The functions related to tooth shape are tooth profile information (Fig. 4.11), tooth shape creation (Fig. 4.12), zoom and distance measurement (Fig. 4.13), and R measurement (Fig. 4.14) as shown in the supplementary form. In addition, there are functions to display and rotate diameter, modification tooth profile, action line, tip width, odd tooth Y measurement.

Item(Division No.)	Symbol	Pinion	Gear
Fillet area	vuf	30	30
Involute area	vui	50	50
Chamfer area	zur	15	15
Tip circle area	vut	10	10
Tooth flank	hul	18	18

Fig. 4.9 Tooth profile computation specification



Fig. 4.10 Meshing drawing & support form

Item	Pinion	Gear
Transverse addendum	6.4000	1.2624
Involute start diameter	64.6870	131.0094
Involute end diameter	79.3564	146.6079
Undercut	No	No

Fig. 4.11 Tooth profile information

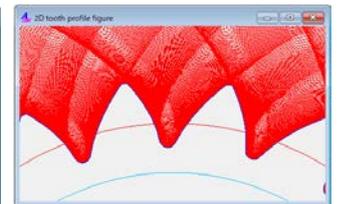


Fig. 4.12 Generation profile

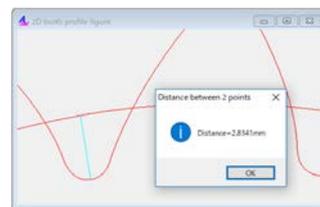


Fig. 4.13 Distance measurement

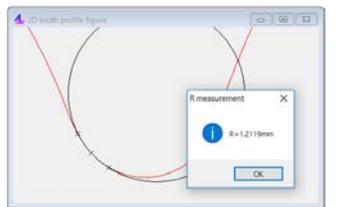


Fig. 4.14 R-measurement

4.7 Teeth profile rendering

The mesh of the 3D tooth profile can be drawn as shown in Figure 4.15, and the contact line can be observed at the mesh. In addition, the direction of the tooth profile can be freely changed by the auxiliary foam, and enlargement, reduction and rotation display of the gear can be displayed.

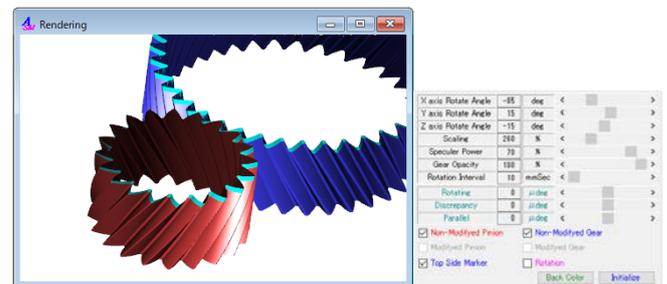


Fig. 4.15 Tooth profile rendering & support form

4.8 Gear accuracy

Figures 4.16 and 4.17 show tolerances for errors according to the new JIS gear accuracy standards JIS B 1702-1: 1998 and JIS B 1702-2: 1998. In addition, it is possible to switch between the new JIS and the old JIS by the settings shown in Figure 4.4. There are the following five types of gear accuracy standards.

- JIS B 1702-1:1998, JIS B 1702-2:1998, JIS B 1702-3:2008
- JIS B 1702:1976
- JGMA 116-02:1983



Fig. 4.16 JIS B 1702-1-2 setting

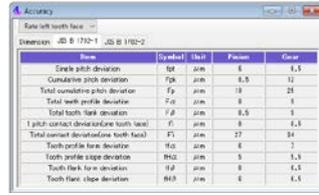


Fig. 4.17 Accuracy tolerance

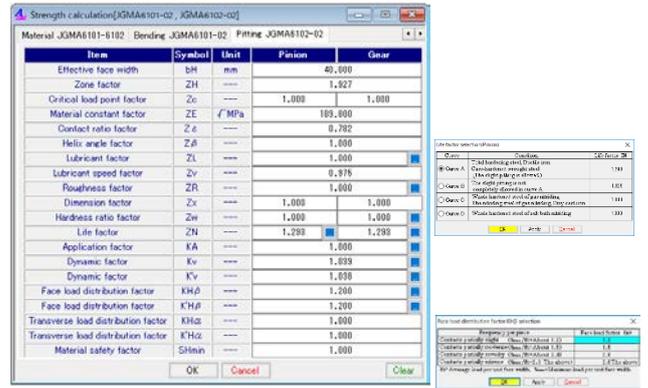


Fig. 4.21 Strength calculation (for pitting factor)

4.9 Gear strength calculation (steel)

The gear strength calculation has "JGMA6101-02:2007" and "JGMA 6102-02:2009" based on "ISO6336:2006" as shown in Fig. 4.5. In addition, there are two types of "JGMA401-01: 1974" and "402-01: 1975". Fig. 4.18 shows the setting screen of strength calculation. In this example, the high-pressure angle side is used as the acting tooth surface, but it is also possible to calculate the strength with the low-pressure angle side as the acting tooth surface. The selection of materials displays a selection form of the materials adapted to "material" and "heat treatment" as shown in Figure 4.19. Fig. 4.20 shows the setting screen for the coefficient related to bending, Fig. 4.21 shows the screen for setting the coefficient related to surface pressure, and Fig. 4.22 shows the strength calculation results.

Note that "..." in the screen is an auxiliary function that allows you to perform numerical conversion, various coefficients, and coefficient selection.

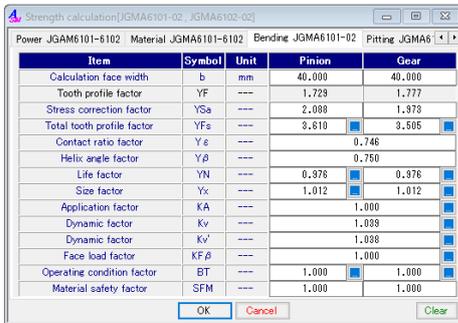


Fig. 4.18 Strength calculation (Power setup)

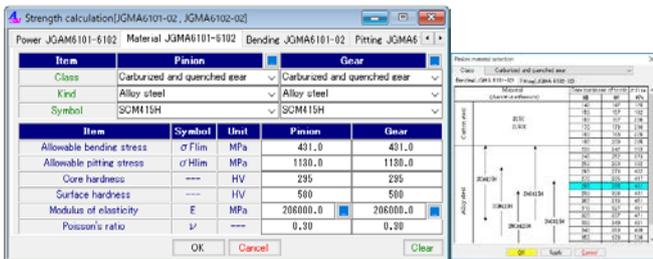


Fig. 4.19 Strength calculation (material)

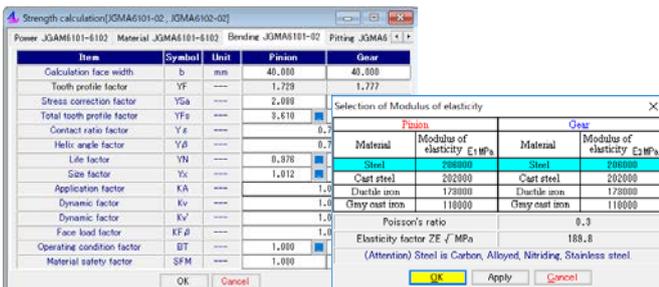


Fig. 4.20 Strength calculation (for bending factor)



Fig. 4.22 Strength calculation result

4.9a Tooth profile factor

The method of calculating the dangerous section tooth thickness when determining the tooth profile factor of a symmetrical tooth gear is defined in each standard, but the dangerous section tooth thickness of the asymmetric tooth gear is not defined. In this software, as shown in Fig. 4.23 and Fig. 4.24, the dangerous section distance on the high-pressure angle side is doubled to be the dangerous section tooth thickness. The load position can be selected from the tip and "HPSTC".

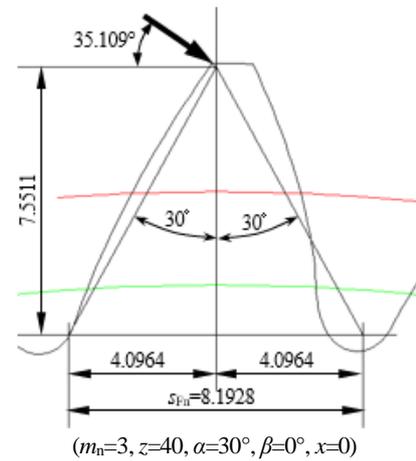
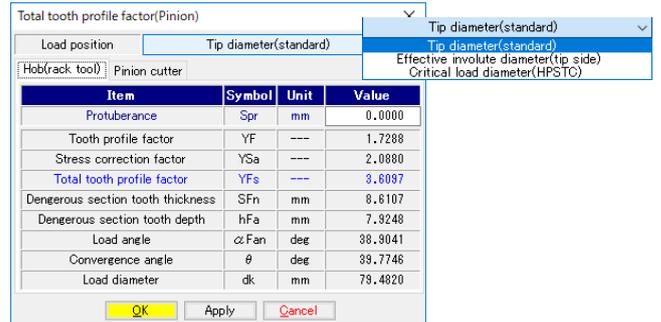


Fig. 4.23 Tooth thickness at critical section (Ex. at Tip load)



The load position can choose at tip or HPSTC.

Fig. 4.24 Tooth form factor

4.10 Gear strength calculation (plastic gear)

The strength of plastic gears can be calculated by selecting JIS B 1759 (2013) in Fig. 4.5. Although JIS B 1759 "Method for evaluating bending strength of plastic cylindrical gears" is not applied to asymmetrical tooth gears, the tooth form factor is calculated as shown in Figure 4.23. The allowable bending stress of plastic material is based on the gear operation test, and the allowable bending stress of POM is determined to be 80.0 [MPa] from the experimental results of various places. Then, the bending stress at the tooth is compared with the allowable bending stress at the tooth taking into consideration various factors (such as shape factor of the base, life factor, temperature coefficient of the atmosphere, etc.). Please see the standard for details. An example of strength calculation of plastic gears is shown in Figure 4.25 to 4.29.

Item	Symbol	Unit	Pinion	Gear
Module	m	mm	1.0000	
Number of teeth	z	---	18	30
Pressure angle(left/right)	α/n	deg	30.0000	17.0000
Helix angle	β	deg	20	0
Helix direction	---	---	Right hand	Left hand
Reference diameter	d	mm	17.02684	31.92533
Base diameter(left/right)	db	mm	14.5074	16.1914
Input type of tooth thickness	---	---	Profile shift coefficient	Profile shift coefficient
Profile shift coefficient	xn	---	0.20000	0.00000
Measurement ball diameter	dp	mm	1.738	1.764
Over ball distance	dm	mm	18.98039	34.48159
Circular tooth thickness	Sn	mm	1.74741	1.57080
Center distance	a	mm	24.80000	
Tooth thinning for backlash	fn	mm	0.00000	0.00000
Face width	b	mm	10.00000	10.00000
Tip diameter	da	mm	18.82684	34.32533
Root diameter	df	mm	14.52684	29.02533
Basic rack root R(left/right)	rf	mm	0.220	0.220

Fig. 4.25 Gear dimensions

Item	Symbol	Unit	Pinion	Gear
Evaluation tooth face	---	---	CCW/left face contact $\alpha/n=30.0000$	
Material	---	---	POM x POM	
Transmission power	P	W	104.7120	
Torque	T	N·m	1.0000	1.8750
Rotational speed	n	min ⁻¹	1000.0000	533.3333
Tangential load	Fwt	N	115.3274	
Tangential velocity	vw	m/s	0.9093	
Transverse contact pressure angle	$\alpha'wt$	deg	32.76441	
Transverse contact ratio	$\epsilon \alpha'$	---	1.3953	
Number of contact	N	---	9999999	
Rim thickness	sR	mm	5.0000	5.0000
Allowable bending stress	σ_{Flim}	MPa	80.018	80.018
Tool tip R(left)	ρ_{fpv}	mm	0.2200	0.2200
Tool tip R(right)	ρ_{fpv}	mm	0.2200	0.2200
Tooth root shape factor	Yf	---	1.000	1.000
Life factor	YNT	---	0.778	0.829
Environment temperature factor	Y θ	---	1.000	
Temperature rising factor	Y $\Delta\theta$	---	0.346	
Lubricant factor	YL	---	1.190	
Mating gear factor	YM	---	0.850	
Minimum safety factor	SFmin	---	1.000	1.000

Fig. 4.26 Strength calculation (Power setup)

Item(Bending)	Symbol	Unit	Pinion	Gear
Bending stress	σ_F	MPa	33.314	31.553
Tooth form factor	YF	---	1.795	1.689
Center location of basic rack-root R	E	mm	-0.179	-0.179
Auxiliary coefficient(For tooth thickness of root dangerous section)	G	---	-1.830	-1.230
Auxiliary angle(For tooth thickness of root dangerous section)	H	rad	-0.860	-0.947
Generative angle of rack tooth(in outer/Root dangerous section location)	θ	rad	0.756	0.685
Tooth thickness of root dangerous section	SFn	mm	2.214	2.382
Arm length of bending moment	hFe	mm	1.462	1.529
Tooth root R	ρ_F	mm	0.484	0.481
Base cylinder helix angle	β_b	deg	17.22940	

Fig.4.27 Strength calculation result

Item(Equivalent spur gear)	Symbol	Unit	Pinion	Gear
Number of teeth	zn	---	18.6543	34.9558
Transverse contact ratio	$\epsilon \alpha'n$	---	1.4627	
Reference diameter	dn	mm	18.6543	34.9558
Normal pitch	pbn	mm	2.7107	
Base diameter	dbn	mm	16.1630	30.5071
Tip diameter	dant	mm	21.4643	37.2956
Diameter of the circle passing through the outer point(One tooth meshing area)	den	mm	18.8951	35.9756
Pressure angle of the outer point(One tooth meshing area)	$\alpha'cn$	deg	35.66382	32.69192
Angle of the outer point(One tooth meshing area)	$\gamma'c$	deg	3.15817	1.68952
Working angle of the outer point(One tooth meshing area)	$\alpha'cn$	deg	32.59565	30.93340

Fig. 4.28 Virtual spur gear

Item(Factor)	Symbol	Unit	Pinion	Gear
Stress correction factor	Ys	---	1.921	1.393
Ratio of arm length(SFn/hFe)	L	---	1.514	1.539
Ratio(σ_{Fn}/ρ_F)	qs	---	2.385	2.384
Helix angle factor	Y β	---	0.833	
Rim thickness factor	YB	---	1.000	1.000
Back up ratio	BR	---	1.887	1.887
Allowable bending stress	σ_{FP}	MPa	45.260	48.539
Safety factor for bending strength	SF	---	1.359	1.538
Safety judgement	---	---	SF > SFmin	SF > SFmin

Fig. 4.29 Factors

4.11 Bearing load

Calculate the load acting on the gear and the load acting on the bearing. The load type calculates 20 types of load acting on each bearing, such as tangential force and normal force. The calculation result is shown in Figure 4.30.

Item(Component)	Symbol	Unit	Pinion	Gear
Tangential load	Ft	N	14204.5455	1099.0000
Normal load	Fn	N	18939.9939	---
Radial load	Fr	N	9489.8970	---
Axial load	Fa	N	8208.9991	---
Radial load(Component)	Fu1(Fu1)	N	7182.2727	7182.2727
Radial load(Component)	Fv1(Fv1)	N	4784.8485	4784.8485
Radial load(Component)	Fu2(Fu2)	N	2886.7619	5773.5627
Radial load(Component)	Fv2(Fv2)	N	7208.7033	12693.3649
Radial load(Component)	Fu3(Fu3)	N	7182.2727	7182.2727
Radial load(Component)	Fv3(Fv3)	N	4784.8485	4784.8485
Radial load(Component)	Fu4(Fu4)	N	2886.7619	5773.5627
Radial load(Component)	Fv4(Fv4)	N	18417.8242	7177.8166

Fig. 4.30 Bearing load

4.12 Tooth surface modification (tooth profile, lead, bias)

An example of tooth surface modification is shown in Figure 4.31. In order to obtain this tooth profile, tooth shape correction can also be given by numerical input as shown in Fig. 4.32. However, it is also possible to input numerical values to the patterned tooth profile as shown on the right. Similarly, lead modification can also be set as shown in Figure 4.33. This tooth profile modification and lead modification can be expressed as shown in Figure 4.34. And if it copies to the opposite tooth side, it will become the same tooth profile of the right and left tooth surface, and if it is combined, it can be displayed as Figure 4.31.

In the combo box at the top of the screen in Fig. 4.34, you can select "Tooth profile", "Lead" and "Tooth profile and Lead". Also, the direction of the tooth profile can be specified by the action line or gear diameter. And, the magnification of tooth profile modification can be set up to maximum 1000 times.

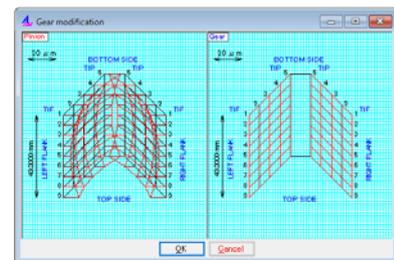


Fig. 4.31 Tooth surface modification (topo graph)

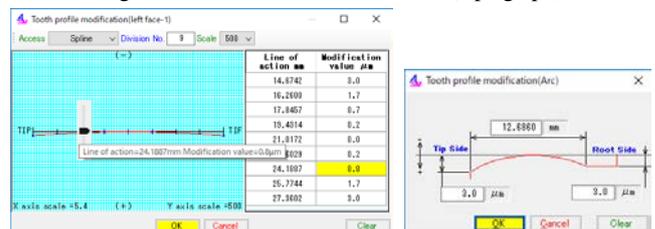


Fig. 4.32 Tooth profile modification

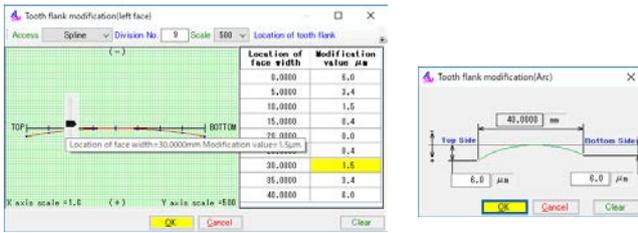


Fig. 4.33 Lead modification

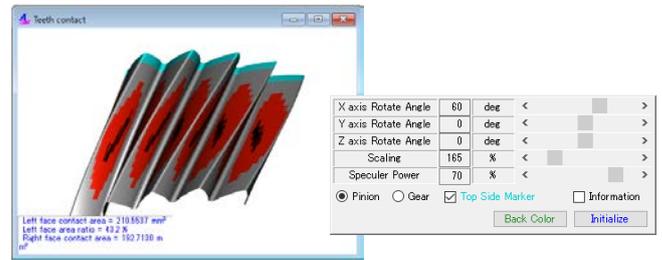


Fig.4.38 Contact pattern (pinion)

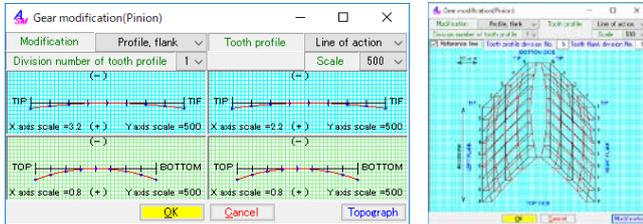


Fig. 4.34 Tooth profile & lead modification, topo graph

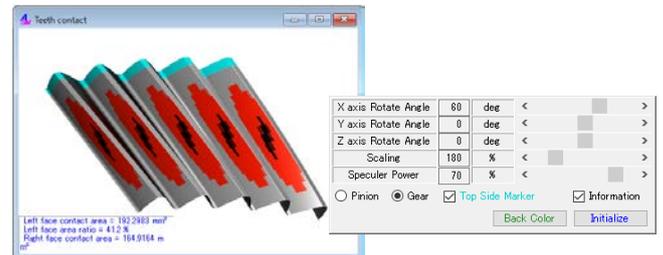


Fig.4.39 Contact pattern (gear)

The tooth profile which has been given tooth surface modification can be set by the tooth profile calculation specifications in Fig. 4.35. The tooth profile calculation conditions set here are valid for the tooth shape shown in Figures 4.10 to 4.14. And this tooth profile can be displayed as shown in Figure 4.36 because it can be superimposed in the rendering in Figure 4.14. Here, the tooth surface is adjusted on the pinion, so the yellow tooth surface appears in the red tooth surface in the figure (the gear is uncorrected).

Item (Division No.)	Symbol	Pinion	Gear
Fillet area	vuf	30	30
Involute area	vui	50	50
Chamfer area	vur	15	15
Tip circle area	vut	10	10
Tooth flank	hul	18	18

Fig. 4.35 Tooth profile calculation

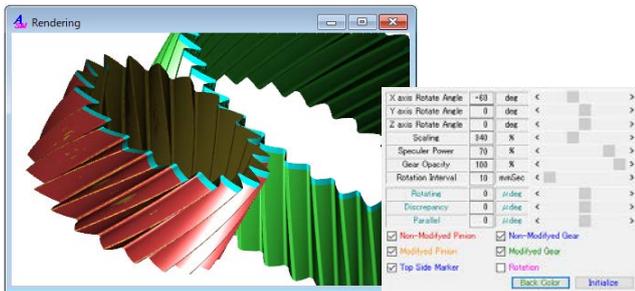


Fig.4.36 Tooth rendering (tooth modification)

4.13 Tooth surface contact

Tooth contact condition can be set in Fig. 4.37 and tooth contact can be confirmed. Here, the tooth contact is shown in Figure 4.38 and Figure 4.39 when the contact clearance is $2.0 \mu\text{m}$ with the parallelism error and the misalignment error as 0.

Item	Symbol	Unit	Value
Center distance	a	mm	105.6000
Parallelism error	p	deg	0.00000
Discrepancy error	di	deg	0.00000
Lead division number	hul	---	18
Tooth profile interpolation accuracy	ac	μm	0,0
Division No. of rotation(per 1 pitch)	urP	---	50
Contact maximum clearance	c	μm	3,0

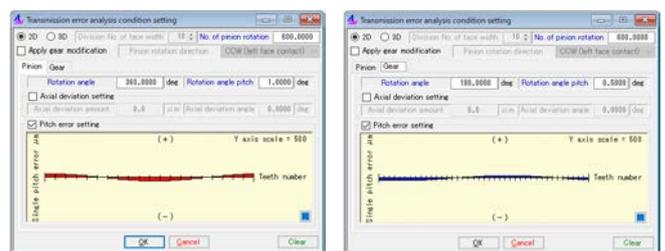
Fig.4.37 Contact analysis setting

4.14 Transmission error

In transmission error analysis, it is possible to perform no-load transmission error analysis with the tooth profile given in Fig. 4.31. Axis deflection and rotational speed can be set with the transmission error setting in Figure 4.40, and 2D analysis or 3D analysis can be performed. Also, the pitch error can be set to the maximum value or the pitch error of all teeth as shown in Figure 4.41.

Transmission error analysis results, CSV File (rotation unevenness) and Fourier analysis results are shown in Figures 4.42 to 4.44. You can also hear [Noise] at in Figure 4.42. Transmission error analysis, wow flutter, and Fourier analysis results can be output to a CSV file as shown in Figure 4.45 using in the lower left of Figure 4.42.

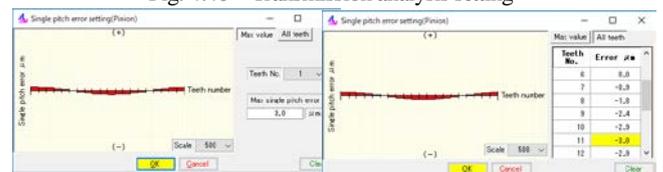
This software is a no-load transmission error analysis. Please use [22] CT-FEM ASM for stress analysis, transmission error analysis and flash temperature analysis corresponding to load and axial angle error.



(a) pinion

(b) gear

Fig. 4.40 Transmission analysis setting



(a) Maxi. value setting

(b) all teeth setting

Fig. 4.41 Pitch error setting

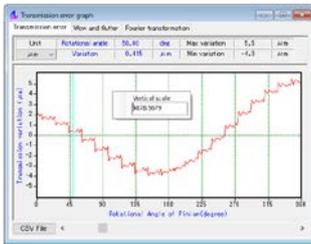


Fig. 4.42 TE result

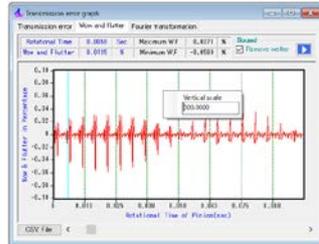


Fig. 4.43 Wow flutter

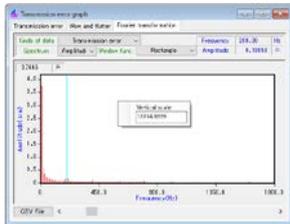


Fig.4.44 Fourier analysis

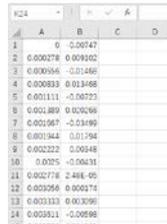


Fig.4.45 csv file example

Item	Symbol	Unit	Pinion	Gear
Module	m	mm	3.00000	3.00000
Number of teeth	z	---	19	55
Pressure angle(left/right)	αzn	deg	30.0000	17.0000
Helix angle	β	deg	0	0.00
Helix direction	---	---	Right hand	Right hand
Reference diameter	d	mm	40.3750	170.9206
Base diameter(left/right)	db	mm	34.6568	146.6248
Input type of tooth thickness	---	---	Profile shift coefficient	Profile shift coefficient
Profile shift coefficient	xn	---	0.30000	0.30000
Measurement ball diameter	db	mm	5.338	5.201
Over ball distance	dm	mm	49.10892	185.05951
Circular tooth thickness	Sn	mm	5.50716	3.91762
Center distance	a	mm	65.00000	65.00000
Tooth thickness for backlash	ln	mm	0.00000	0.00000
Face width	b	mm	25.00000	25.00000
Tip diameter	da	mm	47.67677	167.22057
Root diameter	df	mm	35.57577	179.22057
Basic rack root R(left/right)	r	mm	1.00000	1.00000

Fig. 4.50 Gear dimensions (internal gear)

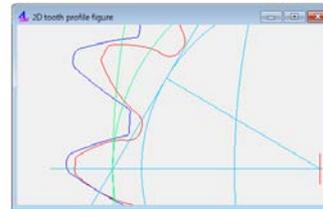


Fig. 4.51 Meshing drawing

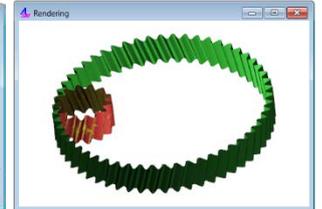
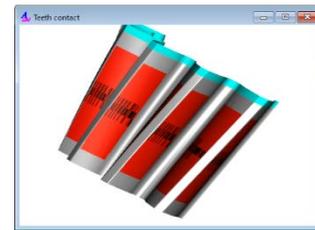
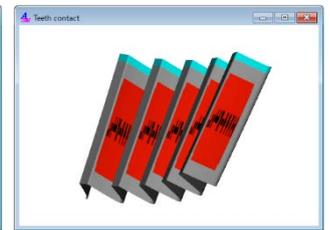


Fig.4.52 Tooth profile rendering



(a) pinion



(b) gear

Fig.4.53 Contact pattern

4.15 Tooth profile output

The generated tooth profile can be output in the tooth profile file format shown in Figure 4.46. In the case of 3D-IGES, output is as shown in Figure 4.47.

In the coordinate correction setting shown in Fig. 4.48, it is possible to output the tooth profile in consideration of use for the mold. As an example, Fig. 4.49 shows a tooth profile (2D) considering a module contraction rate of 20/1000. In addition, tooth profile coordinate values can be output as a text file by "TXT 2D" at the bottom of Fig. 4.46.



Fig. 4.46 Tooth file format

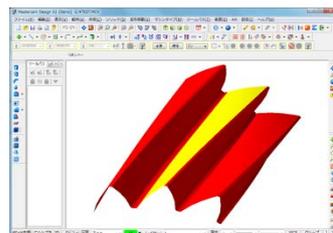


Fig.4.47 CAD sample



Fig.4.48 Coordinate correction setup

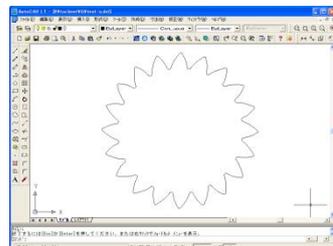


Fig.4.49 CAD sample

4.16 Calculation example of internal gear

The internal gear can be calculated by selecting "External gear × internal gear" in the settings in Figure 4.3. Examples of gear specifications, dimensions, meshing diagrams, tooth profile rendering, and tooth contact are shown in Figures 4.50 to 4.53. The pinion shown in Fig. 4.52 has the same gear face modification as in Fig. 4.31. In addition, strength calculation, transmission error analysis, tooth profile output, etc. are the same as "external gear × external gear".

4.17 FEM tooth profile stress analysis (option)

Examples of FEM analysis are shown in Figure 4.54 and Figure 4.55. The setting method is the same as [1]involute Σ iii (spur and helical gear design system).

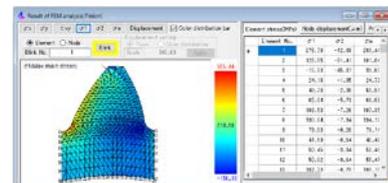


Fig.4.54 FEM (2D), σ_1

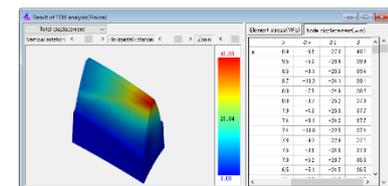


Fig.4.55 FEM (3D), δ_m

4.18 Other

The printing function, [HELP] function, and saving / reading of design data are the same as [1]involute Σ iii (spur and helical gear design system).

Please use [22] CT-FEM ASM for the analysis of 3D stress, tooth surface stress, flash temperature etc. of asymmetric gear.