

[35] K-H-V Differential gear design system

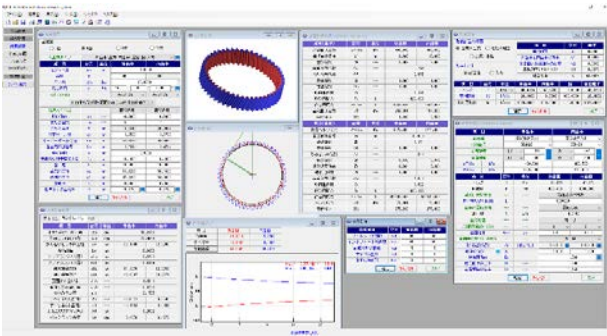


Fig. 35.1 K-H-V Differential gear design system

35.1 Abstract

The K-H-V Differential gear design system is the reduction gear shown in Figure 35.2. The software is a differential reduction (acceleration) mechanism design (three types of gear difference 0, 1 and 2) software for involute gears, and can perform tooth profile design, tooth meshing, sliding ratio, and gear strength calculation. If the difference in the number of teeth is small, involute interference etc. will occur if it is designed with a standard gear with a profile shift of 0. However, with this software, it is possible to calculate gears with combinations of profile shift factor that have a contact ratio of 1 or more and do not generate interference. Please see catalog [34] for differential gear software with trochoid curve.

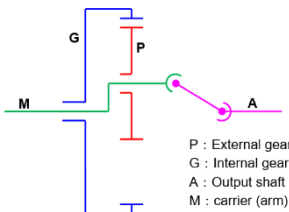


Fig. 35.2 KH-V type reduction mechanism

35.2 Propaty (Basic rack)

As shown in Figure 35.3, set the basic rack and display the actual dimensions of the basic rack set as an auxiliary function.

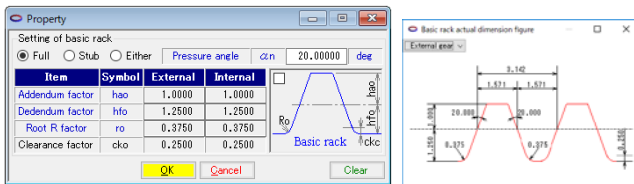


Fig. 35.3 Basic rack

35.2 Gear dimension setting

As shown in Fig. 35.4, select the difference in number of teeth (one tooth difference, two teeth difference, zero tooth difference), and then select the combination (arm fixed / input / output). When the difference in the number of teeth is 0, the tooth shape is drawn with the arm fixed.

After inputting  $m_n$ ,  $z$ ,  $\alpha_n$ ,  $\beta$  in Fig. 35.4, set the profile shift factor ( $x_n$ ). However, there are innumerable ways of giving profile shift factor, so use the auxiliary function shown in Figure 35.3 to determine

combinations with an contact ratio of 1.0 or more and no involute interference. In the case of this example, 55 pieces are displayed. If the profile shift factor No.26 ( $x_{n1} = -0.6$ , ● circle in the figure) is selected from these, the specifications will be determined as shown in Fig. 35.7. The profile shift factor, contact ratio and gear dimensions can be confirmed and selected in the table in Figure 35.6.

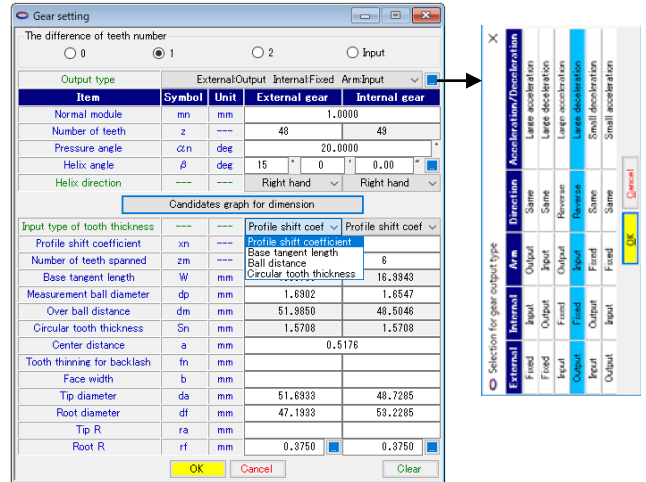


Fig. 35.4 Gear specifications 1

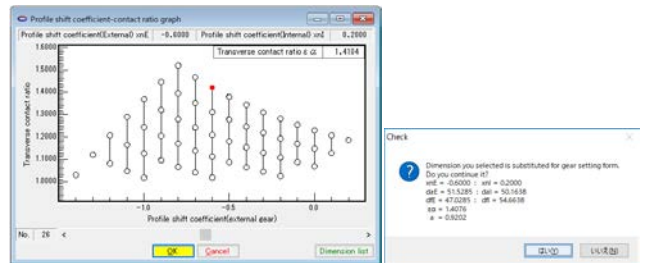


Fig. 35.5 Auxiliary function ( $x_n$  and  $\epsilon$ )

No.	Profile shift coefficient $x_n$	Profile shift coefficient $x_{n2}$	Transverse contact ratio $\epsilon$	Center distance $a$	Tip diameter $d_a$	Root diameter $d_f$
26	-0.6000	0.0000	1.2051	100.00	81.2051	96.7949
27	-0.5000	0.0000	1.2490	100.00	81.2490	96.7510
28	-0.4000	0.0000	1.2929	100.00	81.2929	96.7071
29	-0.3000	0.0000	1.3368	100.00	81.3368	96.6632
30	-0.2000	0.0000	1.3807	100.00	81.3807	96.6193
31	-0.1000	0.0000	1.4246	100.00	81.4246	96.5754
32	0.0000	0.0000	1.4685	100.00	81.4685	96.5315
33	0.1000	0.0000	1.5124	100.00	81.5124	96.4876
34	0.2000	0.0000	1.5563	100.00	81.5563	96.4437
35	0.3000	0.0000	1.6002	100.00	81.6002	96.3998
36	0.4000	0.0000	1.6441	100.00	81.6441	96.3559
37	0.5000	0.0000	1.6880	100.00	81.6880	96.3120
38	0.6000	0.0000	1.7319	100.00	81.7319	96.2681
39	0.7000	0.0000	1.7758	100.00	81.7758	96.2242
40	0.8000	0.0000	1.8197	100.00	81.8197	96.1803
41	0.9000	0.0000	1.8636	100.00	81.8636	96.1364
42	1.0000	0.0000	1.9075	100.00	81.9075	96.0925
43	1.1000	0.0000	1.9514	100.00	81.9514	96.0486
44	1.2000	0.0000	1.9953	100.00	81.9953	96.0047
45	1.3000	0.0000	2.0392	100.00	82.0392	95.9608
46	1.4000	0.0000	2.0831	100.00	82.0831	95.9169
47	1.5000	0.0000	2.1270	100.00	82.1270	95.8730
48	1.6000	0.0000	2.1709	100.00	82.1709	95.8291
49	1.7000	0.0000	2.2148	100.00	82.2148	95.7852
50	1.8000	0.0000	2.2587	100.00	82.2587	95.7413
51	1.9000	0.0000	2.3026	100.00	82.3026	95.6974
52	2.0000	0.0000	2.3465	100.00	82.3465	95.6535
53	2.1000	0.0000	2.3904	100.00	82.3904	95.6096
54	2.2000	0.0000	2.4343	100.00	82.4343	95.5657
55	2.3000	0.0000	2.4782	100.00	82.4782	95.5218

Fig. 35.6 Auxiliary function (No. 27,  $x_n$  and  $\epsilon$ )

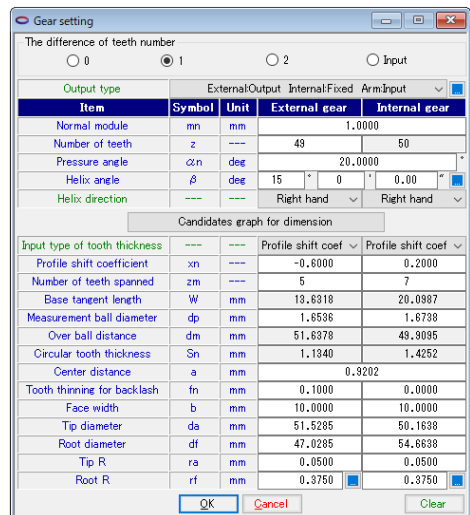


Fig. 35.7 Gear specifications 2

When the gear specifications in Fig. 35.7 are confirmed, dimensions and interference calculation results are displayed as in Fig. 35.8 to Fig. 35.10. In the case of this example, although the trimming has occurred, the calculation will proceed as it is because there is no influence on the mesh.

Item	Symbol	Unit	External gear	Internal gear
Transverse module	mt	mm		1.0353
Transverse pressure angle	$\alpha_t$	deg		20.6469
Reference diameter	d	mm	49.8933	50.7285
Base diameter	db	mm	46.5015	47.4703
Base cylindrical helix angle	$\beta_b$	deg		14.0761
Lead	pz	mm	582.8327	594.7709
Maximum effective diameter	dh	mm	51.4712	54.2727
Minimum effective diameter(TIF)	dt	mm	47.8875	50.2310
Cutting profile shift coefficient	xnc	---	-0.7462	0.2000
Tooth depth	h	mm	2.2500	2.2500
Design normal circular tooth thickness	sn'	mm	1.0276	1.4252
Design over ball distance	dm'	mm	50.2857	48.0479
Design base tangent length	W	mm	19.5163	20.0833

Fig. 35.8 Gear basic dimensions

Item	Symbol	Unit	External gear	Internal gear
Transverse contact pressure angle	$\alpha_w$	deg	58.2378	
Contact helix angle	$\beta_w$	deg	25.4693	
Contact pitch diameter	dw	mm	88.3392	90.1798
Effective face width	bw	mm		10.0000
Clearance(large diameter)	ckh	mm		0.6474
Clearance(small diameter)	ckl	mm		0.6474
Maximum contact diameter	dja	mm	51.4723	59.0278
Minimum contact diameter	djf	mm	48.8185	50.2319
Transverse contact ratio	$\epsilon_{\alpha}$	---		1.1840
Overlap contact ratio	$\epsilon_{\beta}$	---		0.8238
Total contact ratio	$\epsilon_{\gamma}$	---		2.0078
Sliding ratio(large diameter)	$\sigma_a$	---	-0.0491	0.0468
Sliding ratio(small diameter)	$\sigma_f$	---	-0.0827	0.0784
Transverse backlash	jnt	mm		0.1031
Backlash angle	j $\sigma$	deg	0.2542	0.2490

Fig. 35.9 Gear contact dimensions

Item	Symbol	Unit	External(Output)	Internal(Fixed)	Arm(Input)
Rotation ratio	Vhi	---	-0.0208	0.0000	1.0000
Reverse rotation ratio(=1/Vhi)	Uhi	---	-48.0000	0.0000	1.0000
Trimming				occurs(Attention)	
Involute interference				doesn't occur(Safety)	
Trochoid interference				doesn't occur(Safety)	
Fillet interference				doesn't occur(Safety)	

Fig. 35.10 Gear interference

### 35.4 Tooth profile

The tooth profile of the gear specifications (Fig. 35.7) can be drawn as shown in Fig. 35.11. Figure 34.12 shows a close-up view of the tooth profile (A) and (B). Also, distance measurement is possible as shown in Figure 34.12 (b). Figure 35.14 shows teeth rendering.

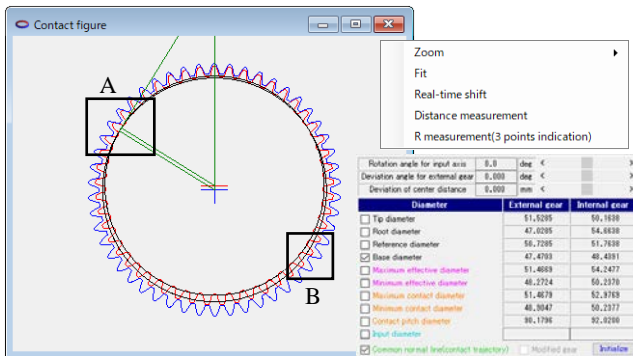
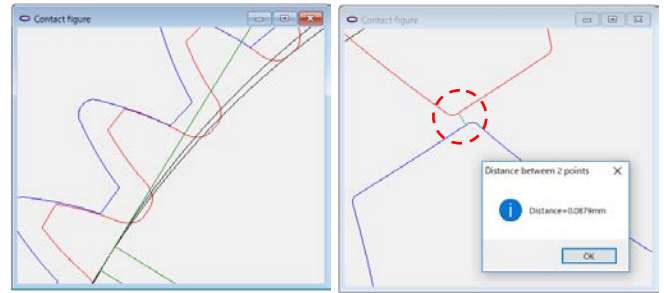


Fig. 35.11 Gear mesh diagram



(a) A part (b) B part

Fig. 35.12 Gear mesh diagram, distance measurement

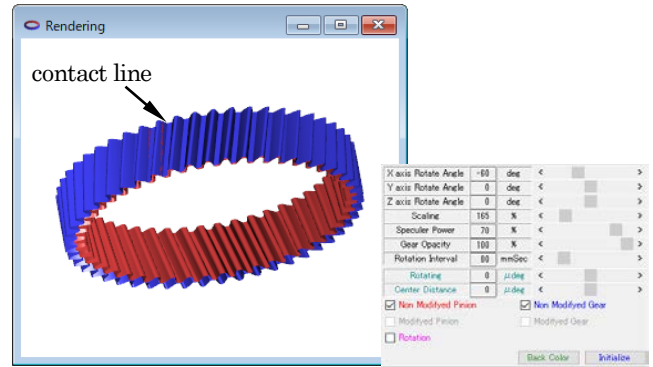


Fig. 35.13 Tooth rendering, tooth profile, rotation

### 35.5 Tooth profile / tooth lead modification (option)

When modifying tooth profile and tooth lead, you can apply modifications as shown in Fig. 35.149~35.16. In Figure 35.16, you can enter a specified number of points (maximum = 50) to be modified, and you can also enter an arc pattern. Then, the contact of the modified tooth profile can be confirmed as shown in Figure 35.17.

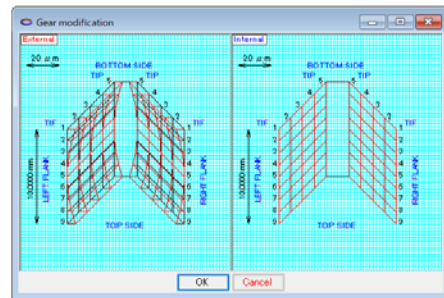


Fig. 35.14 Tooth rendering, tooth profile and topograph

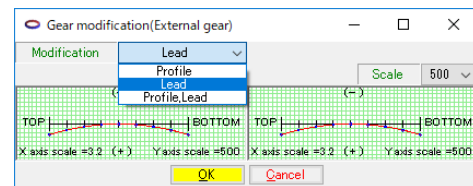


Fig. 35.15 Tooth lead input example

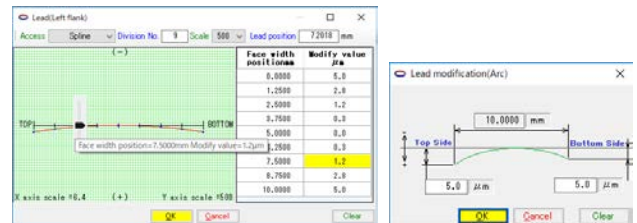


Fig. 35.16 Tooth lead input and arc input example

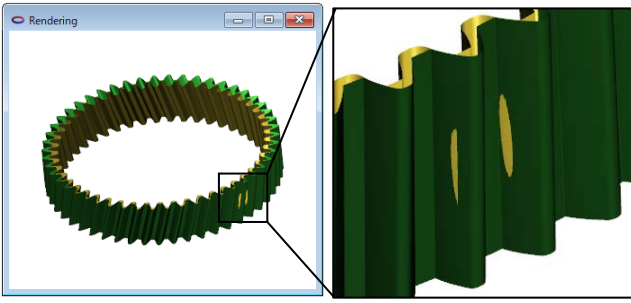


Fig. 35.17 Tooth rendering, modified tooth form

### 35.6 Sliding ratio

The sliding ratio of this example gear is shown in the dimension calculation result of Fig. 35.9, and the change of the sliding ratio at the tooth profile position (roll angle) is shown in Fig. 35.18.

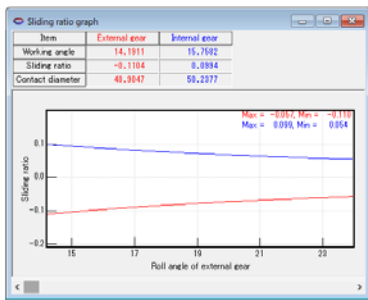


Fig. 35.18 Sliding ratio

### 35.7 Gear strength

For gear strength calculation, enter the coefficient of friction, torque and rotational speed on the strength setting screen as shown in Figure 35.19. In this example, when the coefficient of friction is 0.10, the input torque of the arm is 1 (Nm), and the rotational speed is 1000 min<sup>-1</sup>, the torque and rotational speed of the pinion and gear are displayed with the [OK] button.

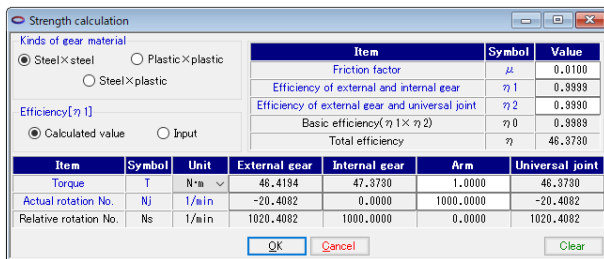


Fig. 35.19 Gear strength calculation specification setting

The input screen of gear strength specifications (materials, factors) is shown in Figure 35.21. Material selection can be made from the table in

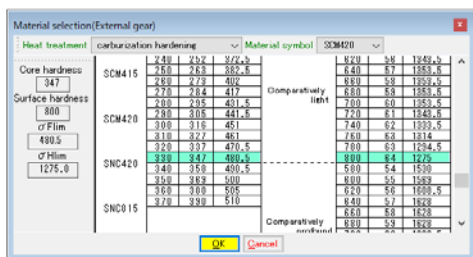


Fig. 35.20 Selection of material

Figure 35.20, but you can also input  $\sigma_{Film}$  and  $\sigma_{Hlim}$  directly. Figure 35.22 shows the gear strength results.

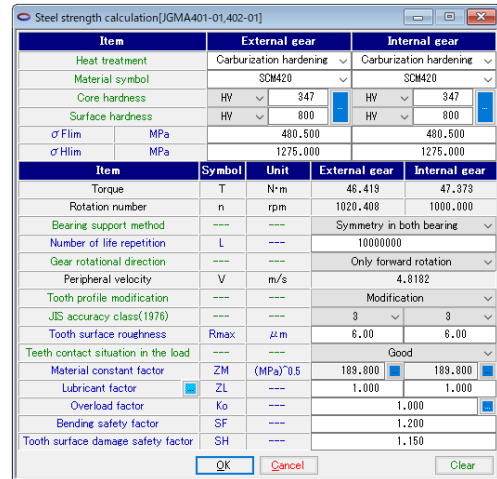


Fig. 35.21 Gear strength calculation (strength specification)

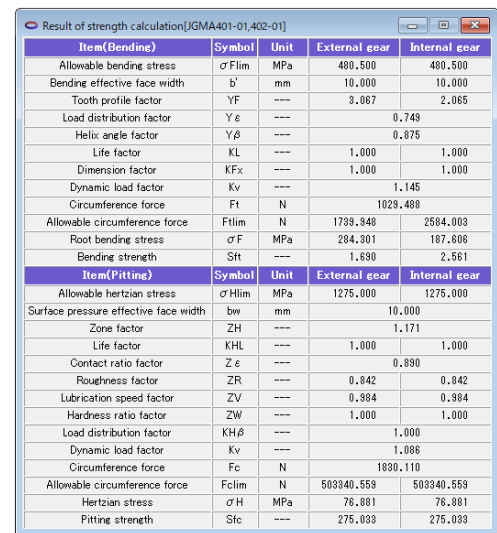


Fig. 35.22 Gear strength result

### 35.8 Tooth profile output

The generated tooth profile can be output as CAD data. Figures 35.24 and 35.25 show examples of drawing CAD data output by the tooth profile output function shown in Figure 35.23.



Fig. 35.23 Tooth profile output

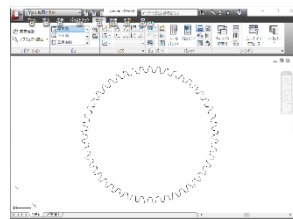


Fig. 35.24 CAD example (2D)

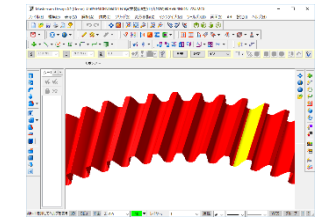


Fig. 35.25 CAD example (3D)

### 35.9 Design example of the difference in number of teeth 0

An example of the gear mechanism (K-H-V) connected in two stages is shown in Figure 35.26. The 1st gear is an external and internal gear with one tooth gap (internal gear fixed, external gear output, arm input). The 2nd stage (follower side) is an external / internal gear with a zero-tooth difference. By connecting the 1st stage external gear and the 2nd stage internal gear, output can be made on the same axis as the input axis.

In Figure 35.26, none of the external gear, internal gear and arms in the second step, with 0-tooth difference, is fixed. The rotation ratio of the driven side of the green (differential external gear + internal gear with zero tooth difference) and the external gear (red) of the red is the same. Therefore, it is possible to take out the reduction ratio of the differential gear coaxially. The following is a design example of a zero-tooth differential gear.

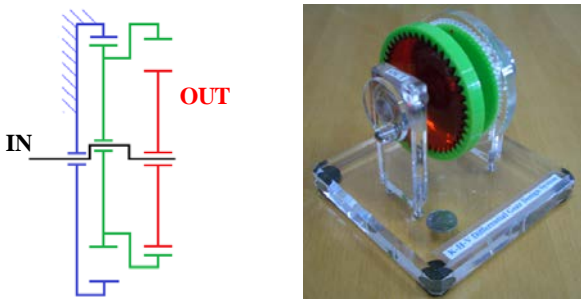


Fig. 35.26 Mechanism (1st stage differential, 2nd stage  $z_1=z_2$ ), model

In Fig. 35.27, select 0 in gear number difference, and set the module, number of teeth, pressure angle and helix angle. Next, select No. 25 out of 25 items that fit in the auxiliary function (Fig. 35.28). The dimensions of this gear are shown in Fig. 35.29 and in Fig. 35.30. Also, Fig. 35.31

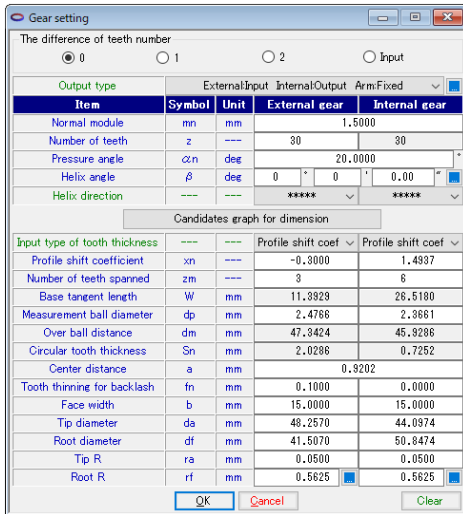


Fig. 35.27 Gear specification setting

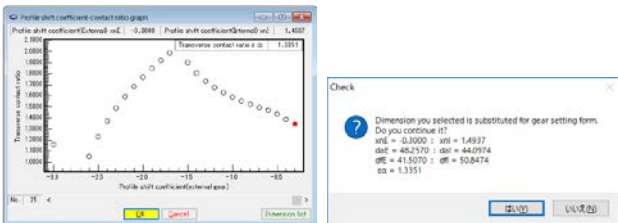


Fig. 35.28 Auxiliary function ( $x_n$  and contact ratio)

shows an enlarged view of the meshing parts C and D in Fig. 35.30. Teeth rendering is shown in Figure 35.32.

Dimension	Contact	Interference	External gear	Internal gear
Transverse contact pressure angle	$\alpha_w$	deg	30.0000	
Contact helix angle	$\beta_w$	deg	---	
Contact pitch diameter	dw	mm	---	---
Effective face width	bw	mm	15.0000	
Clearance(large diameter)	ckh	mm	0.3750	
Clearance(small diameter)	ckt	mm	0.3750	
Maximum contact diameter	dja	mm	48.2048	49.1149
Minimum contact diameter	djf	mm	43.6726	44.1686
Transverse contact ratio	$\epsilon_\alpha$	---	1.2972	
Overlap contact ratio	$\epsilon_\beta$	---	0.0000	
Total contact ratio	$\epsilon_\gamma$	---	1.2972	
Sliding ratio(large diameter)	$\sigma_a$	---	-0.0795	0.0797
Sliding ratio(small diameter)	$\sigma_f$	---	-0.1696	0.1449
Transverse backlash	jnt	mm	0.1000	
Backlash angle	$j\sigma$	deg	0.2711	0.2711

Fig. 35.29 Gear contact dimensions

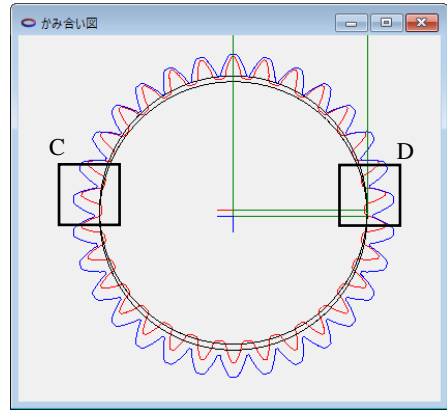


Fig. 35.30 Gear mesh diagram ( $z_1=z_2$ )

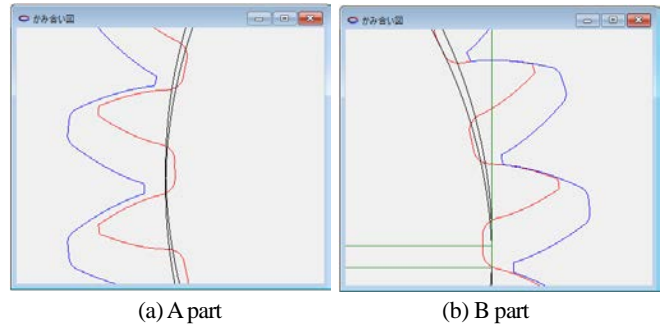


Fig. 35.31 Gear mesh diagram (zoom)

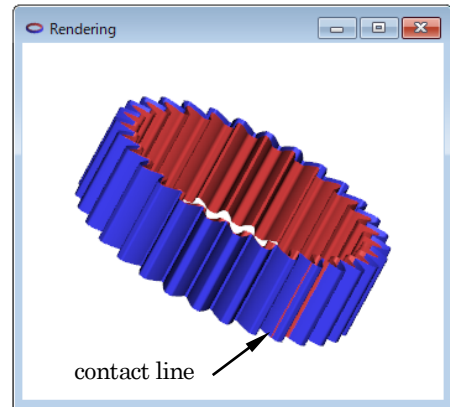


Fig. 35.32 Teeth rendering